



<http://www.cnrs-orleans.fr/icare/>
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Review of ICARE-CNRS activities on facilitating CO₂ capture from the combustion of fossil fuels

Centre National de la Recherche Scientifique - CNRS
**Institut de Combustion, Aérothermique,
Réactivité et Environnement - ICARE**

Iskender GÖKALP
Director

Outline

- Few words about ICARE-CNRS @ Orléans
- Basic chemical kinetic studies on the oxydation of methane, ethylene and propene in the presence of CO₂ and H₂O (ANR project TACOMA)
- Combustion of methane in oxygen enriched air coupled with membrane capture of CO₂. Basic and pilot system studies (CNRS Energy Program project COCASE)
- Retrofitting a pulverised coal power plant into a oxyfuel system. (FP7 TREN demonstration project SOMALOX)
- Interdisciplinary and comparative analyses of the acceptability of new energy technologies: the case studies of CCS in France and Canada (CNRS Energy Program project ALICANTE)
- 10th ICCEU

ICARE in Orléans

- Institut de
 - Combustion
 - Aérothermique
 - Réactivité et
 - Environnement
-
- Institute for Combustion, Aerothermal sciences, Reactivity, Environment



Where is ICARE ?



ICARE is in Orléans,
125 km from Paris

ICARE - CNRS

Institut de Combustion, Aérothermique
Réactivité et Environnement
1c, avenue de la Recherche Scientifique
45071 Orléans - Cedex 2 - France

Total staff : 120

26 Researchers and faculty
21 Engineers and technicians
39 PhD students and post-docs
34 Various trainees



Main research domains and areas



Two main research domains:

Energy & Environnement
Space & Propulsion

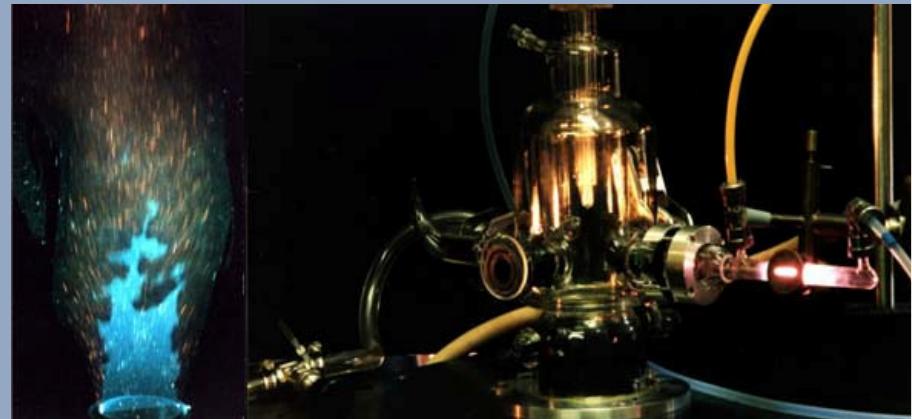
Four main research thematics:

Chemical kinetics of combustion and reactive systems
Dynamics of combustion and reactive systems
Atmospheric chemistry
Supersonic, hypersonic, rarefied, ionized flows

Research domains of ICARE

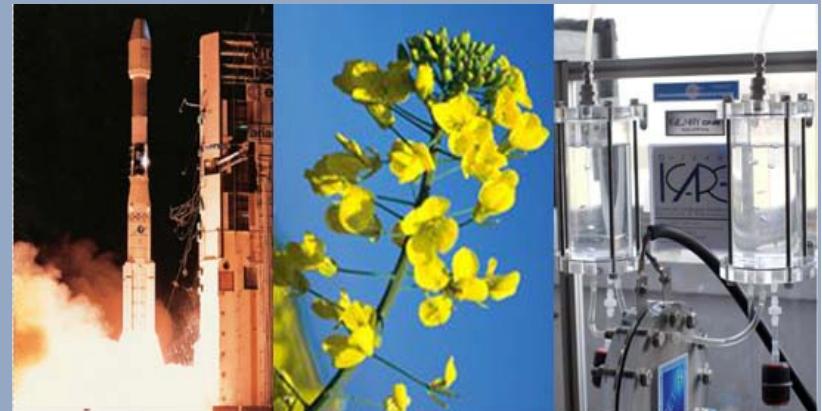
Energy & Environment Propulsion & Space

- Combustion
- Chemical kinetics
- Plasmas physics
 - Fluid mechanics, turbulence
 - Two phase flows
 - Supersonic, hypersonic flows
 - Ionized, rarefied flows

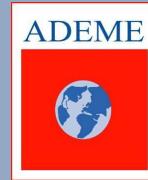


Application domains

- Aerospace propulsion
- Electric propulsion
- Liquid and solid propulsion
- Atmospheric reentry
- Atmospheric chemistry
- Energy production
- Alternative fuels, biofuels, hydrogen
- Pollutant emissions reductions
- Industrial risk prevention



Main contractual cooperations



esa



INERIS

IRSN
INSTITUT
DE RADIOPROTECTION
ET DE SÛRETÉ NUCLÉAIRE

AREVA



Main international cooperations: UE, Russie, USA, Canada, Chine, Japon, Ukraine, Turquie, Argentine, etc

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Project TACOMA (GDF SUEZ; TOTAL; IFP; ICARE-CNRS)

- A new combustion mode for glass, petrochemistry, steel industries to concentrate CO₂ in the flue gases
- Combustion of heavy oil and natural gas diluted with recirculation of burnt gases
- Ethylene and propene are the main products of the cracking of heavy oil
- Oxydation of C₂H₄ and C₃H₆ in O₂/N₂/CO₂/H₂O at atmospheric pressure, over a wide range of initial concentrations, temperatures and equivalence ratios. A detailed chemical kinetic reaction mechanism was used to simulate the experiments and analyze the results.

Project TACOMA-ICARE CNRS

Conclusions

- The oxidation of ethylene is inhibited by water and the effect decreases with the increasing equivalence ratio. Carbon dioxide accelerates slightly the consumption of C₂H₄ under fuel-rich conditions. The oxidation of ethylene in presence of water vapor yields reduced formation of carbon monoxide and increased acetylene production. Carbon dioxide participates to the production of CO when initially present in ethylene-O₂-N₂ reacting mixtures.
- The oxidation of propene is less affected by the presence of CO₂ or H₂O in the reacting mixture under the present JSR conditions.

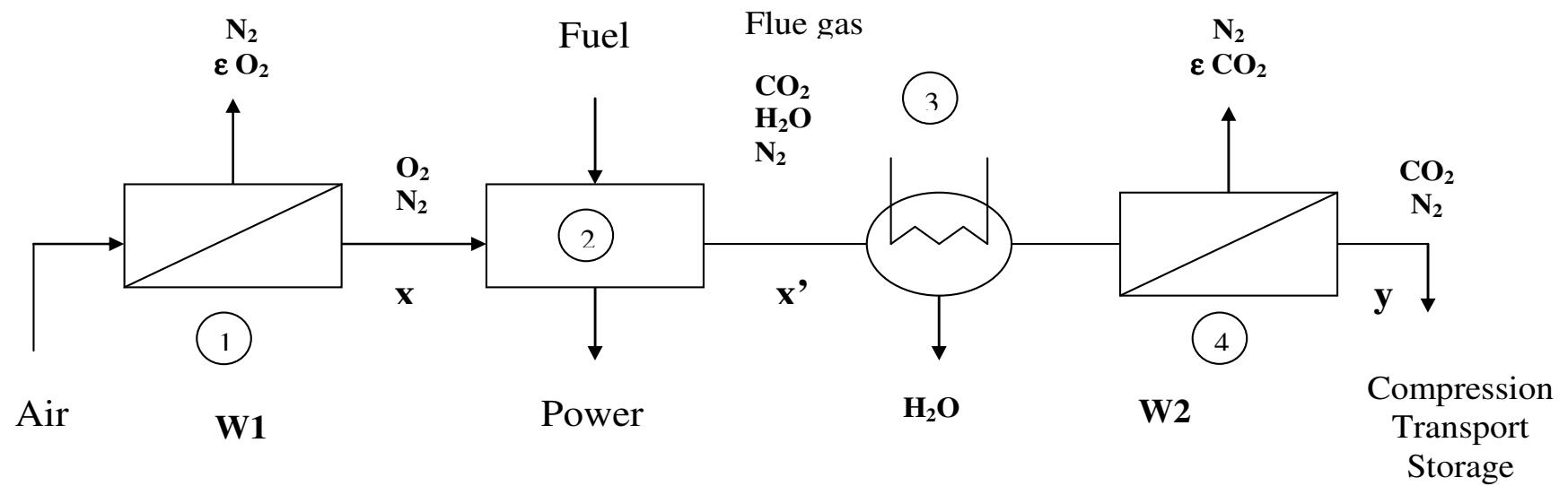
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Oxygen enriched air combustion of methane in relation with membrane capture of CO₂ Project COCASE (CNRS Energy Program)

- Membrane capture of CO₂ is a promising technology but needs a minimum of 20% CO₂ concentration in the flue gases.
- Combustion of CH₄ in oxygen enriched air with CO₂ recirculation is investigated to optimise the O₂ concentration, the CO₂ recirculation rate, the CO₂ concentration rate and the membrane properties

Project COCASE: Global principle

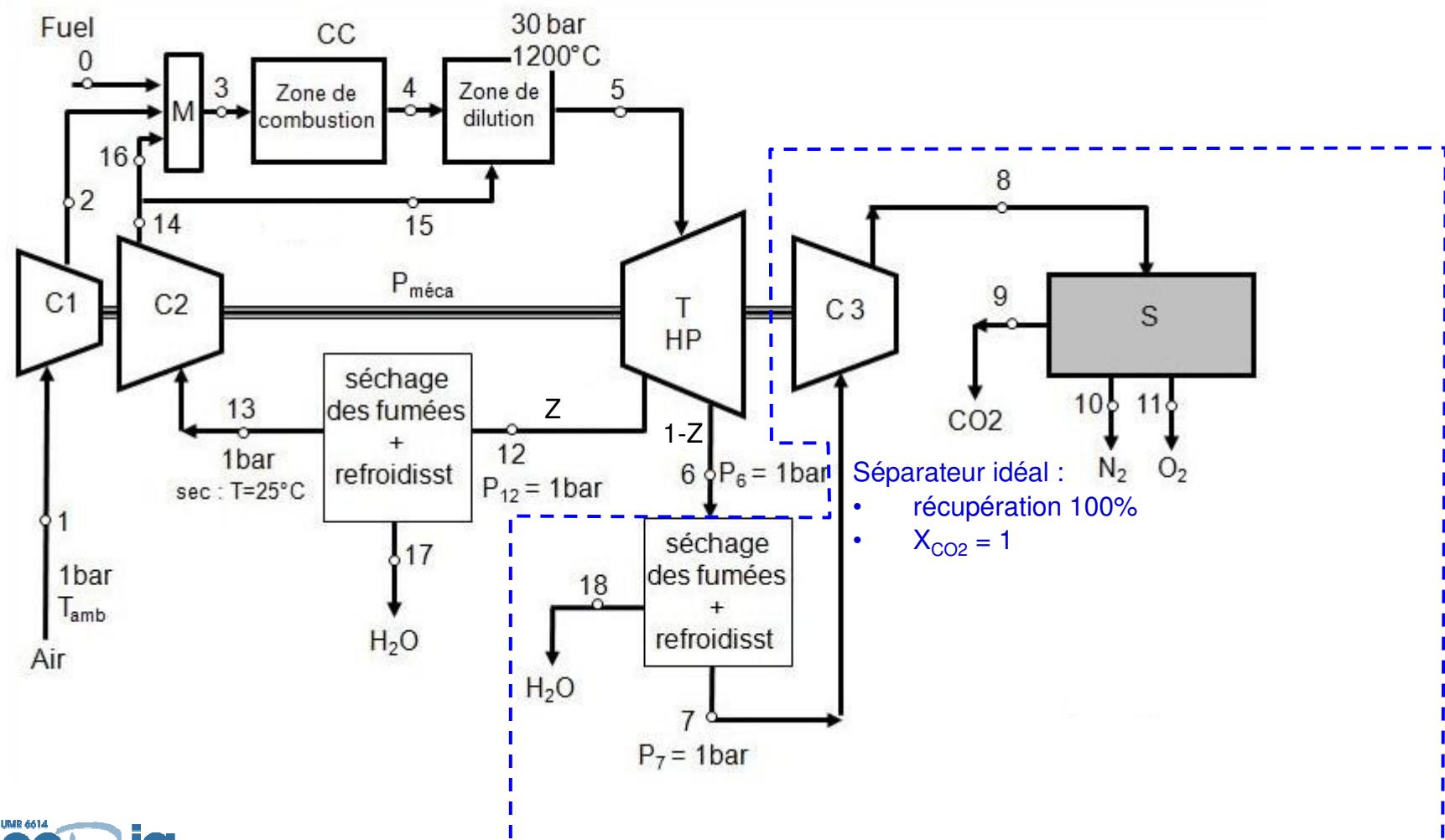


Impact énergétique de la récupération du CO₂

Cycle turbine réaliste + recyclage + recompresion - capture CO₂(idéal)

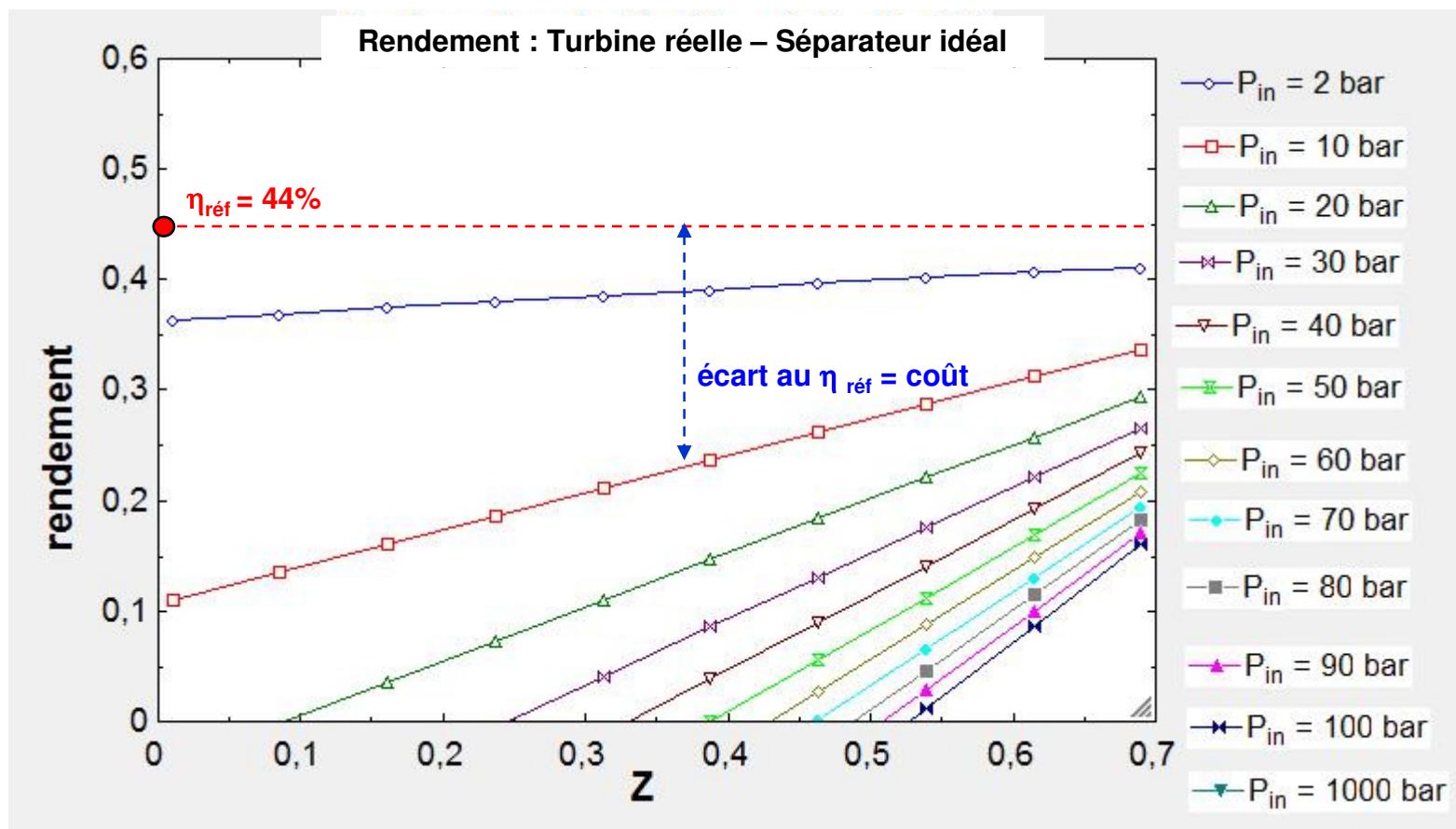
: P₃ = HP= 30bar, P₁=P₂ = P_{atmo}, T₄ = 1200°C

$\eta_{\text{is-comprimeur}} = 0.9$, $\eta_{\text{is-turbine}} = 0.9$, $\Delta P_{\text{Ch Comb}} = 5\%$



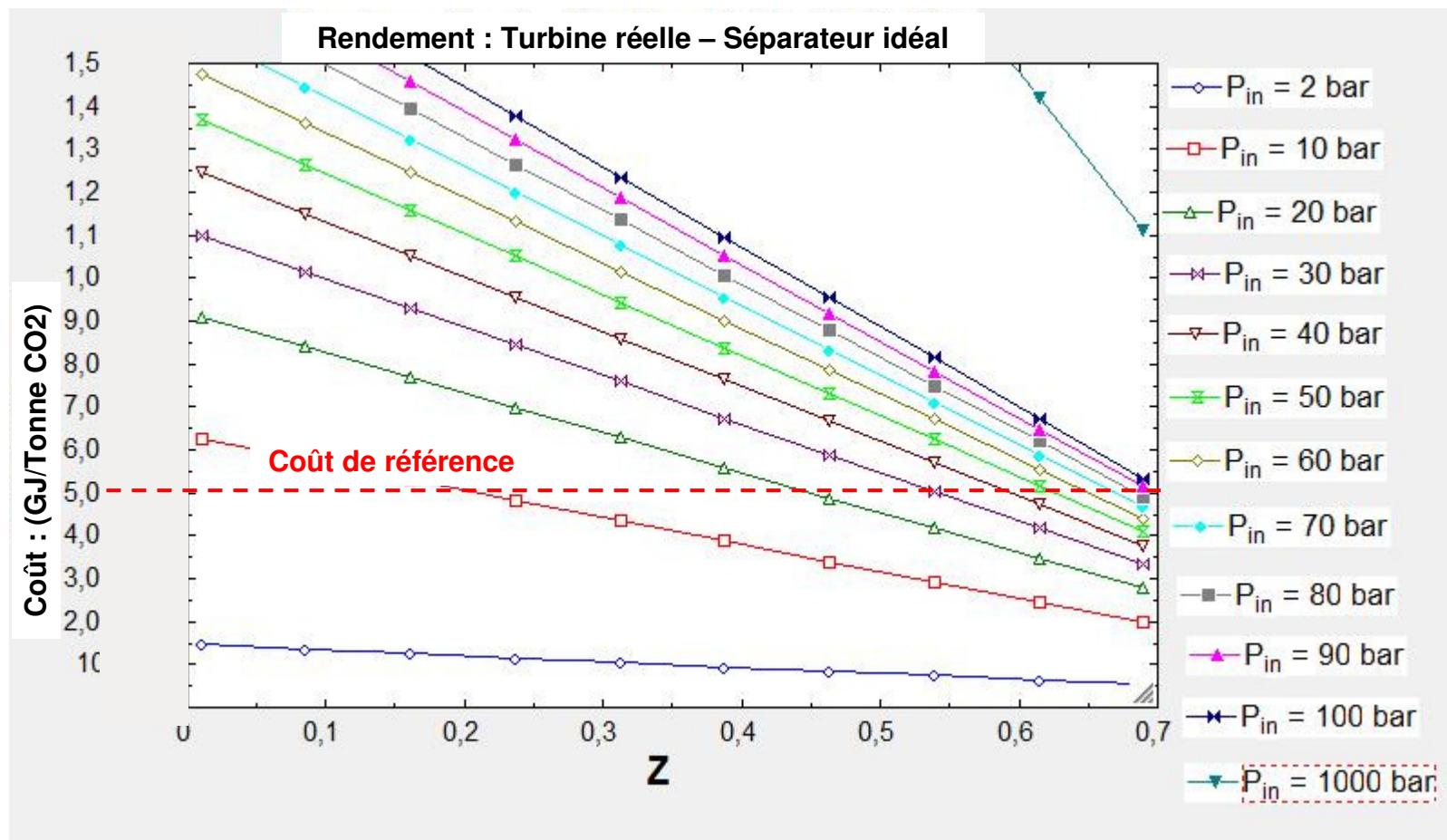
Impact énergétique de la récupération du CO₂

Impact du taux de recirculation Z et de la pression P_{in} en entrée du séparateur sur le rendement



Impact énergétique de la récupération du CO₂

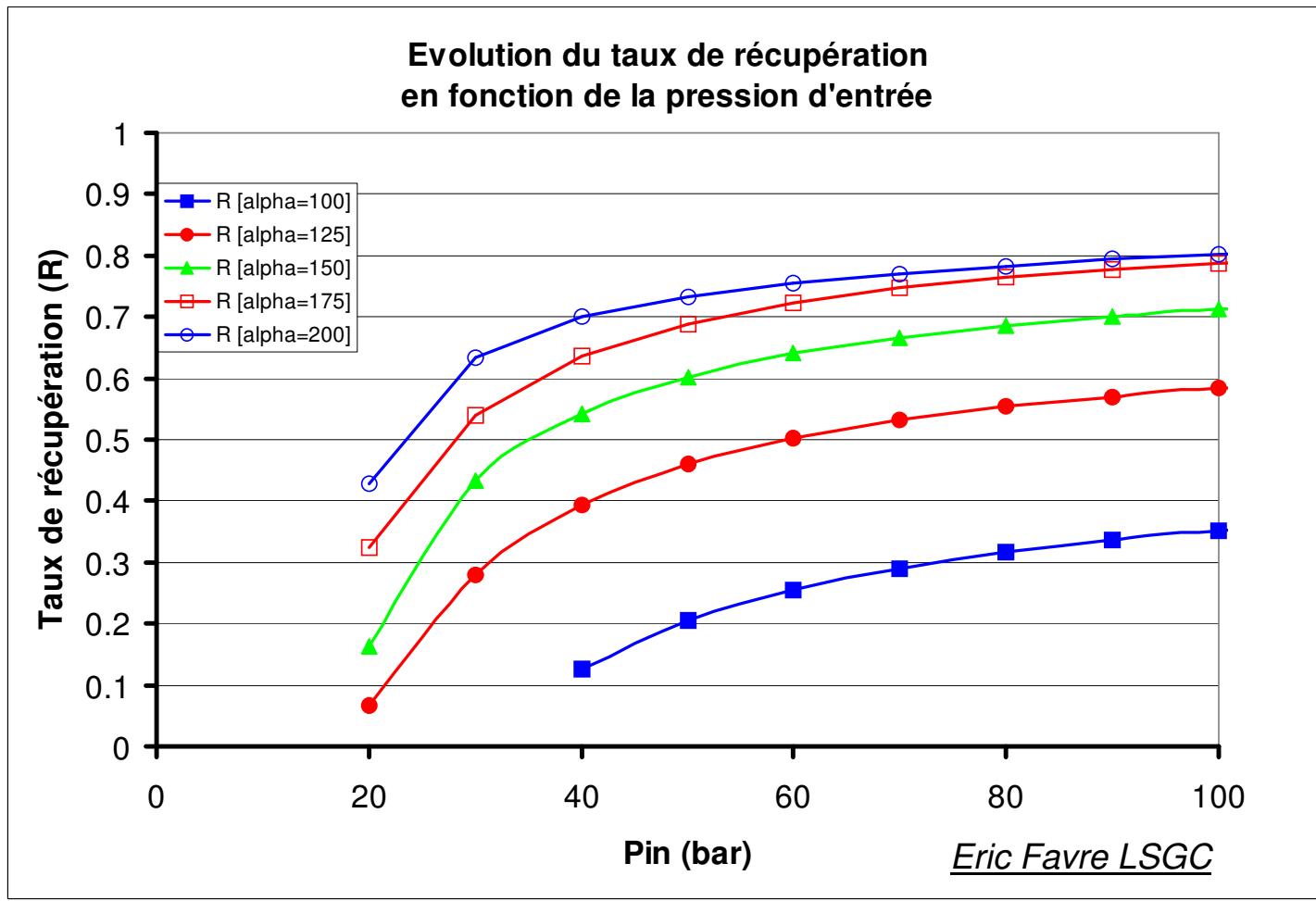
Impact du taux de recirculation Z et de la pression P_{in} en entrée du séparateur sur le cout de capture du CO₂



Impact énergétique de la récupération du CO₂

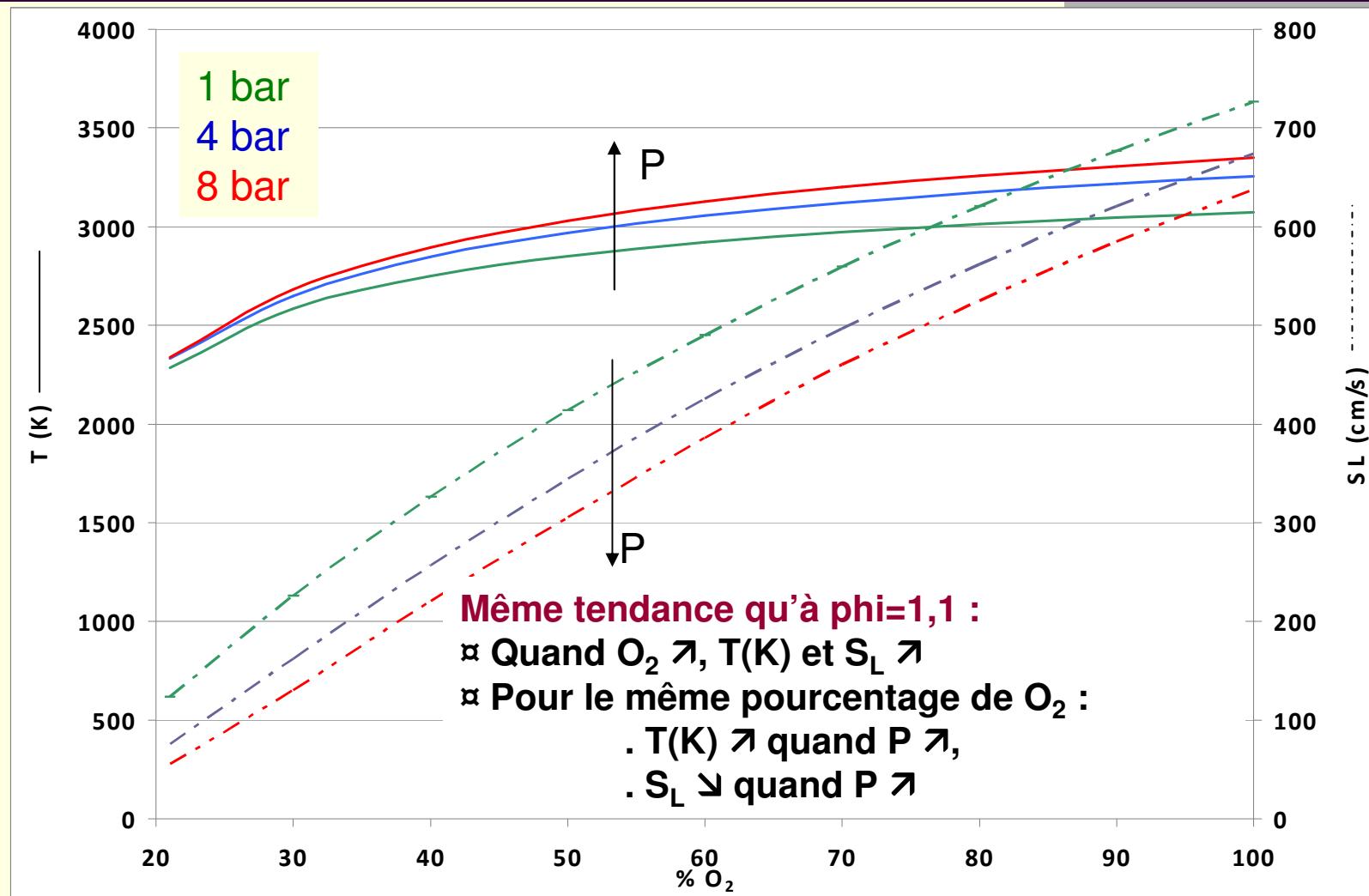
Taux de récupération de la membrane
en fonction de la sélectivité de la membrane et de la pression Pin (entrée membrane)

X_{in} = 0.11 maximale avec taux de recirculation maximale (0.7)
 X_{out} = 0.9



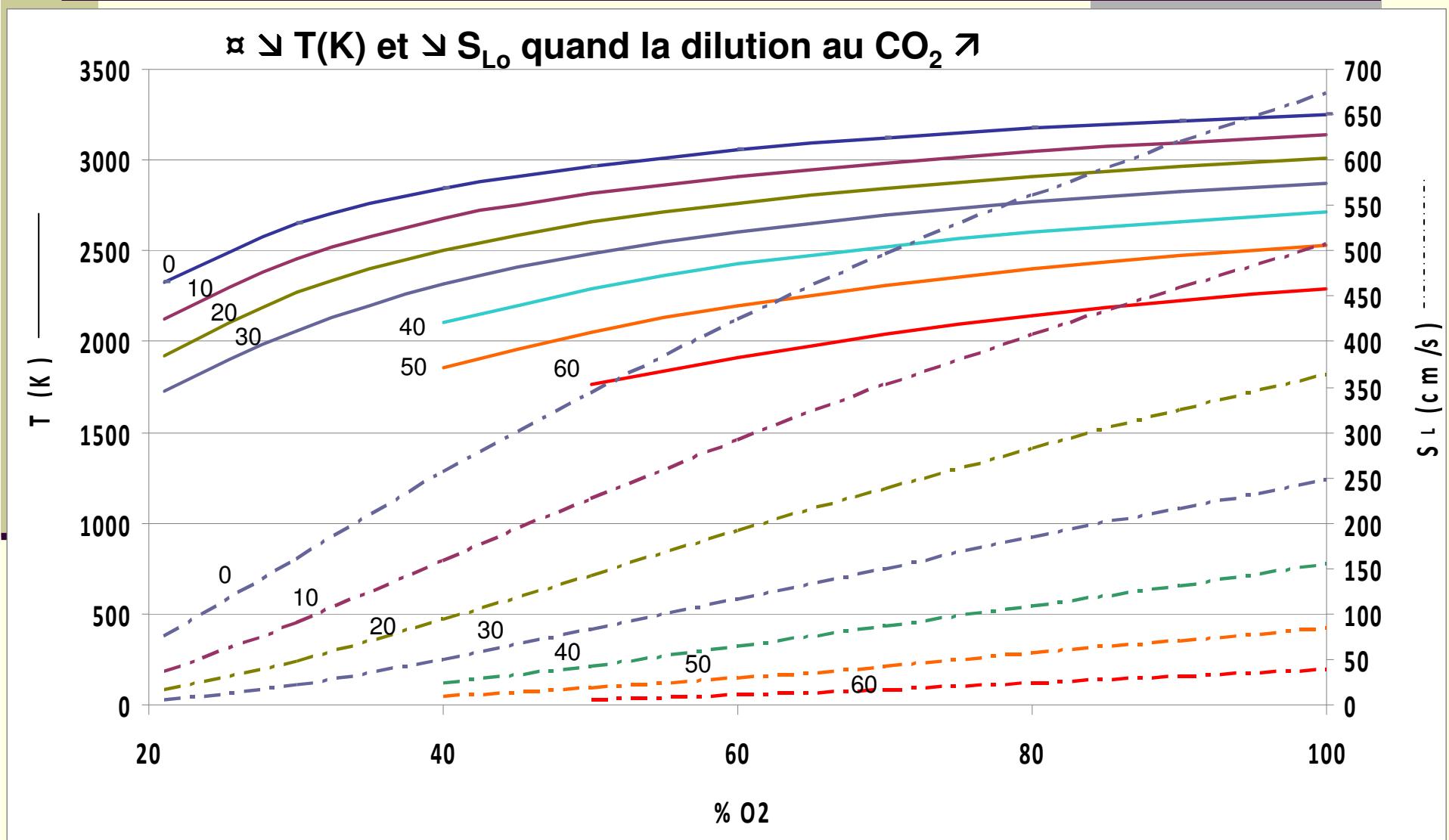


Résultats à $\phi=0,9$ (condition n°1 : enrichissement seul)
Température et vitesse de flamme en f° du %O₂ dans l'air (1, 4, 8 bars), T_o=600K



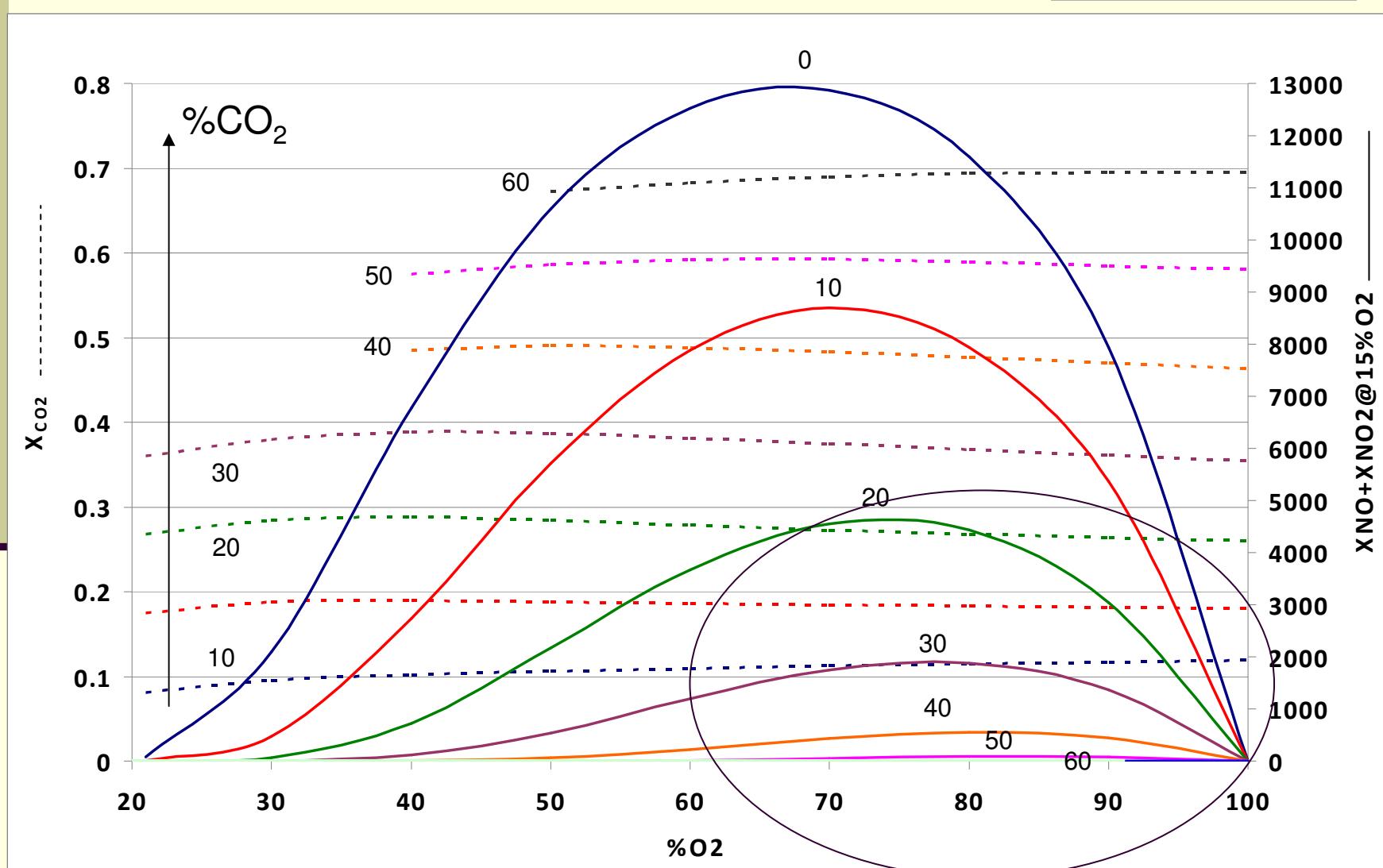
Résultats à phi=0,9 :

Température et vitesse de flamme en f° du %O₂ dans l'air, T_o=600K, avec ou sans dilution (4 bars)



Résultats à phi=0,9 :

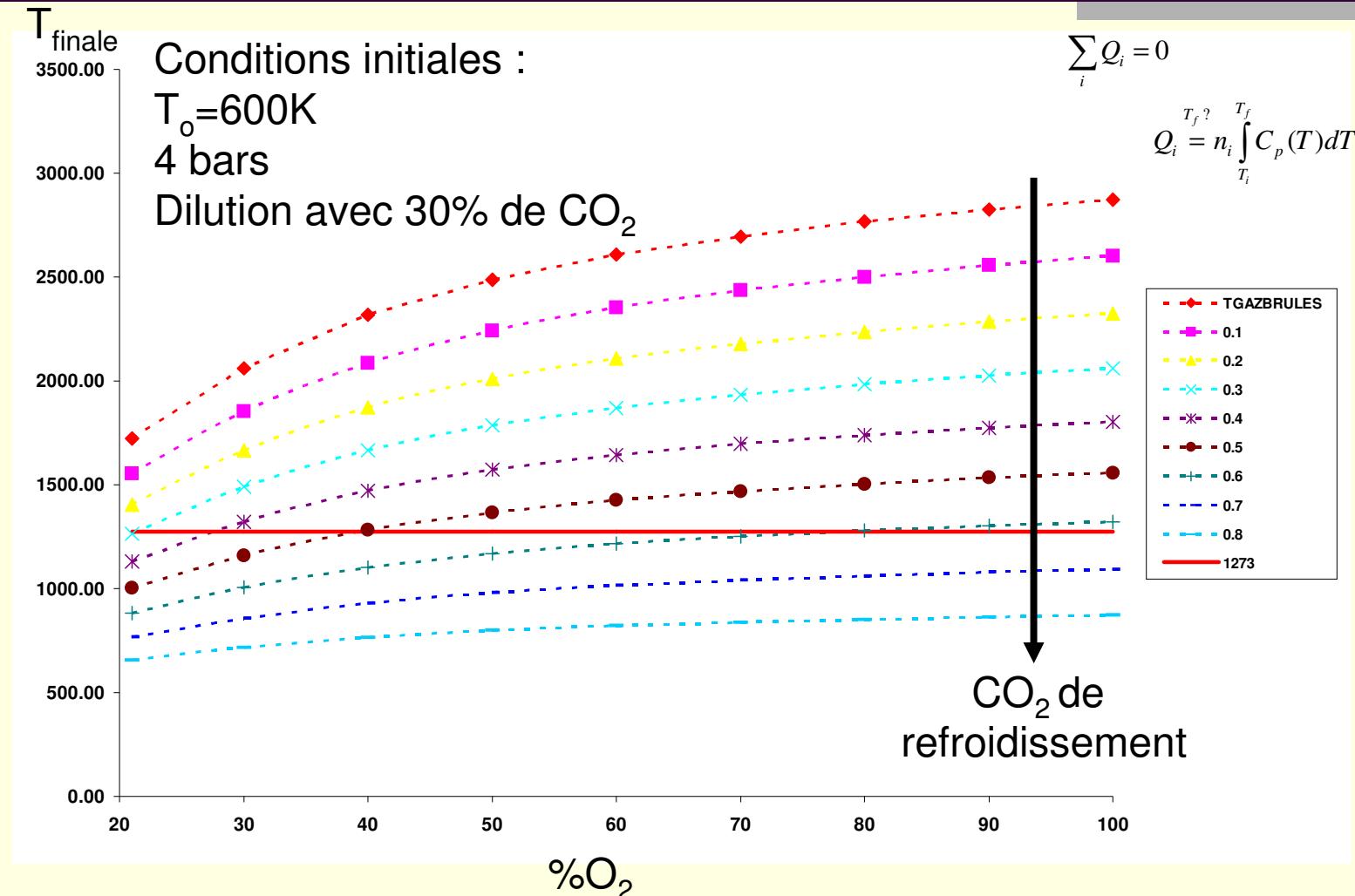
CO_2 et NOx (Thomsen) en f° du % O_2 dans l'air, $T_o=600\text{K}$, avec ou sans dilution (4 bars)





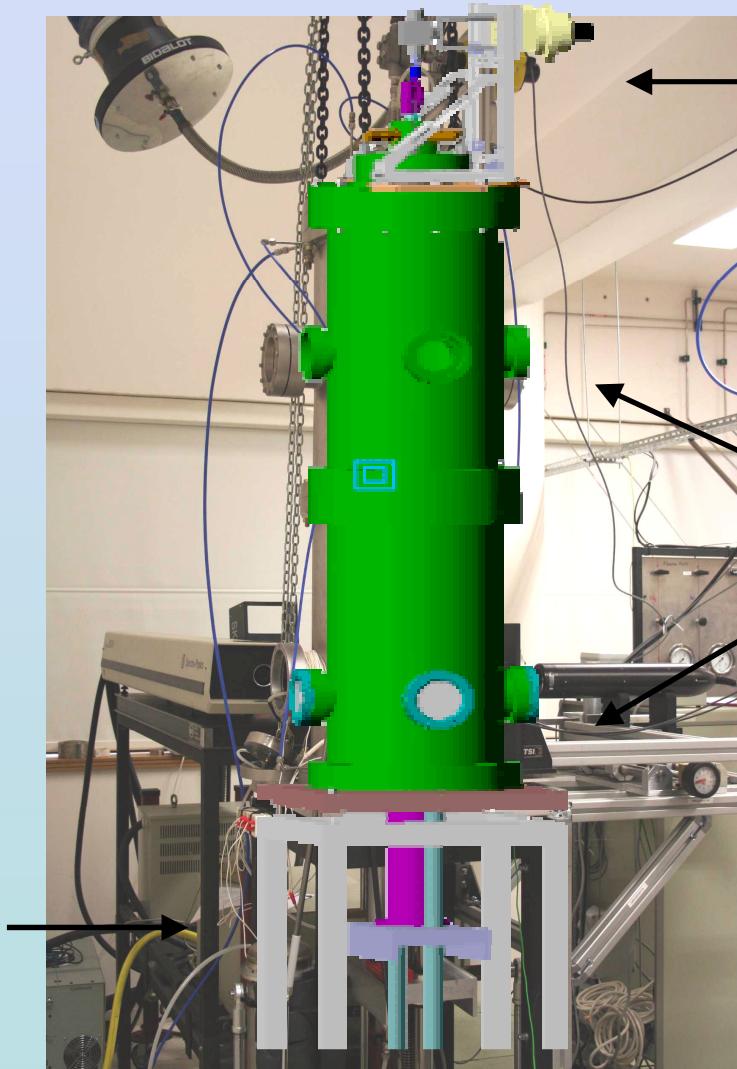
Résultats à phi=0,9 :

Refroidissement : environ 60% de CO₂ froid (300K) nécessaire quelle que soit la pression et les conditions



High Pressure Chamber

- $H = 1.2 \text{ m}$
- $D_{\text{int}} = 0.3 \text{ m}$
- Water cooling system
- Windows heating system
- Laser light absorbing paint



Axial
displacement

Pressure
regulation

Windows

Laminar Burner

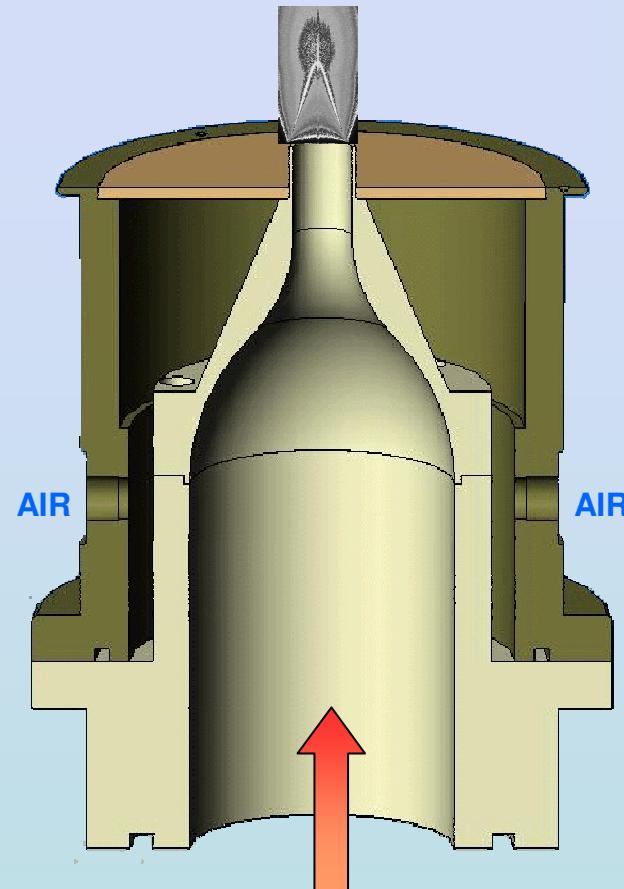


Experimental conditions

- $U_0 = 0.7 \text{ à } 1 \text{ m/s}$
- $\phi = 0.9 \text{ à } 1.05$
- $P < 0.2 \text{ MPa}$
- $Re < 1300$

Characteristics

- Bunsen Burner
- $D = 12 \text{ mm}$



Objectives

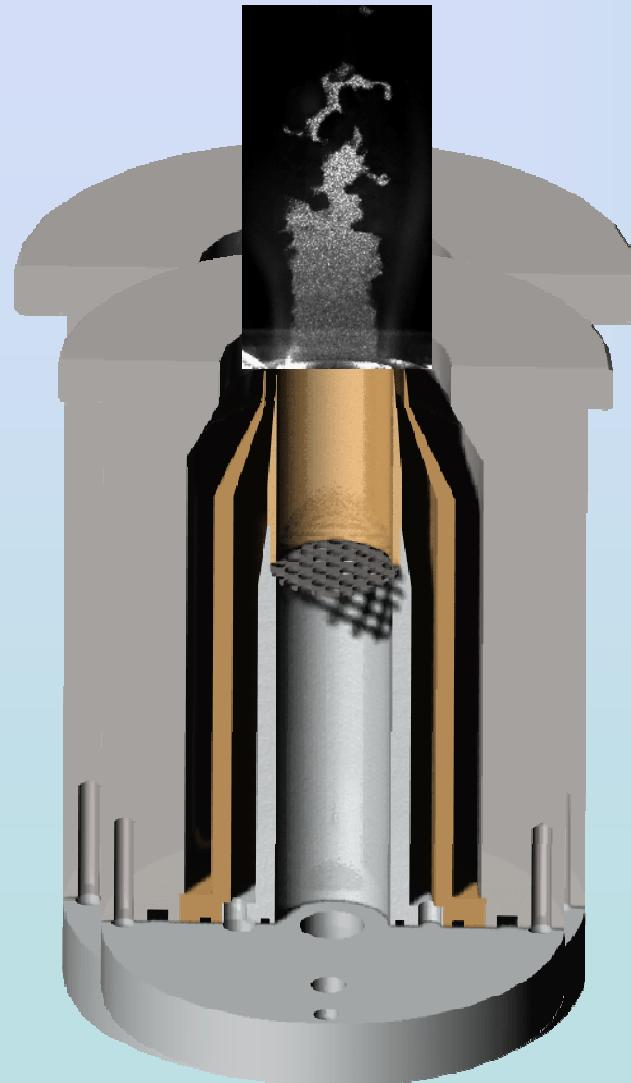
Study of the Flickering

High Pressure

Turbulent Burner

Experimental conditions

- $U \approx 2.1 \text{ m/s}$
- $\phi = 0.6 \text{ à } 0.7$
- $P = 0.1 \text{ à } 0.9 \text{ MPa}$
- Pilot flame flow $< 7\%$
Main flow
- $T = 300 \text{ K}$
- u' et L_U cste



Flow conditions

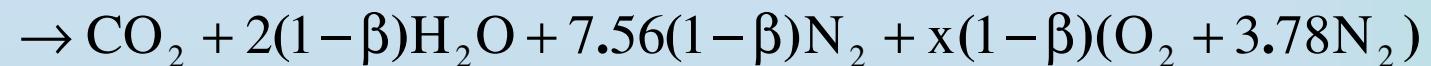
- Mean flow velocity :

- $U_0 = 0.7$ to 1 m/s (Laminar)
 - $U \approx 2.1$ m/s (Turbulent)

- Equivalence ratio :

- $\phi = 0.9$ to 1.05 (Laminar)
 - $\phi = 0.6$ (Turbulent)

- CO_2 addition :



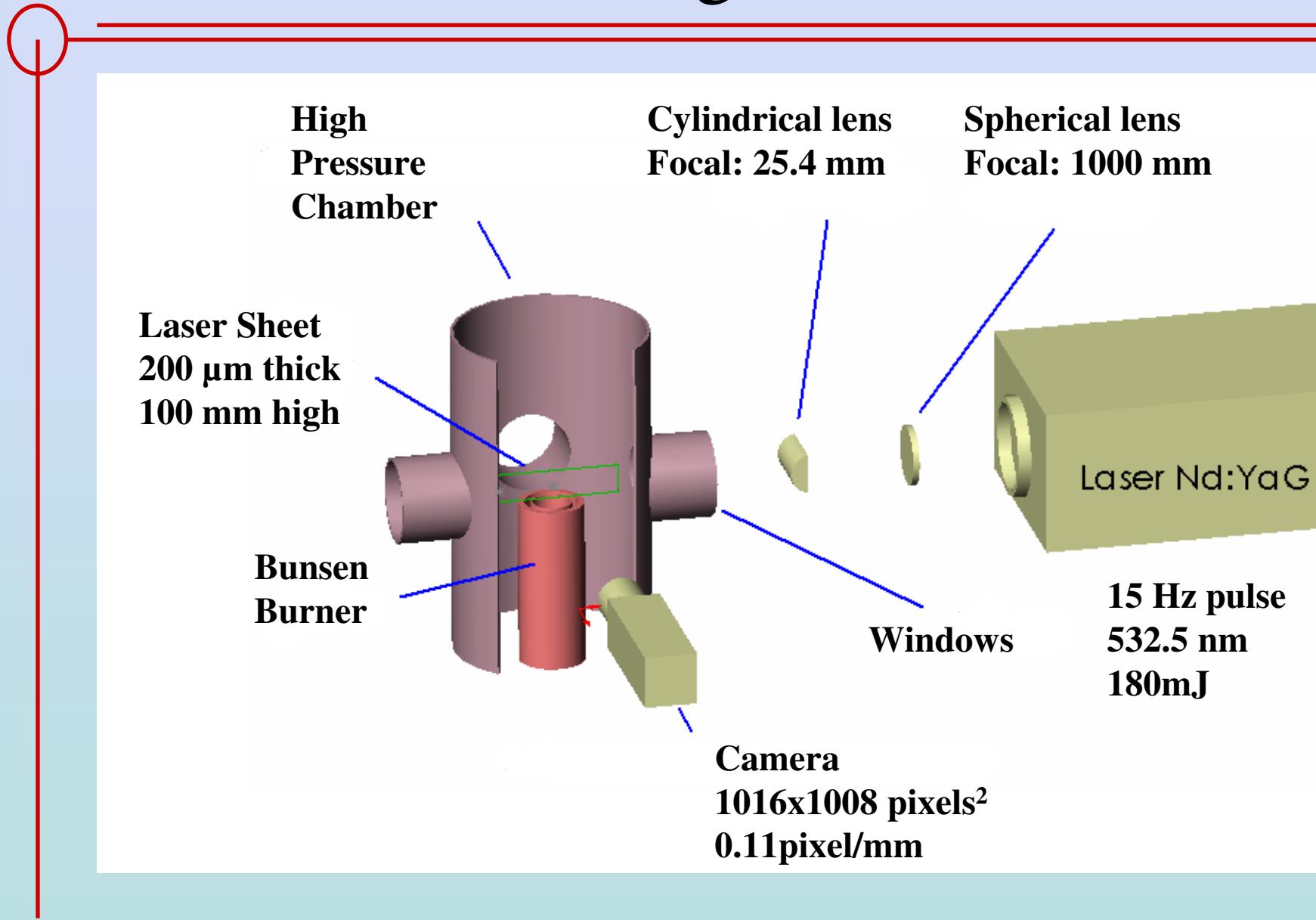
where $\beta = \frac{n(\text{CO}_2)}{n(\text{CH}_4) + n(\text{CO}_2)}$ and x the air excess

- Pressure :

- $P < 0.2$ MPa (Laminar)
 - $P < 0.9$ MPa (Turbulent)

- Temperature of fresh gases : 300 K

Laser diagnostics



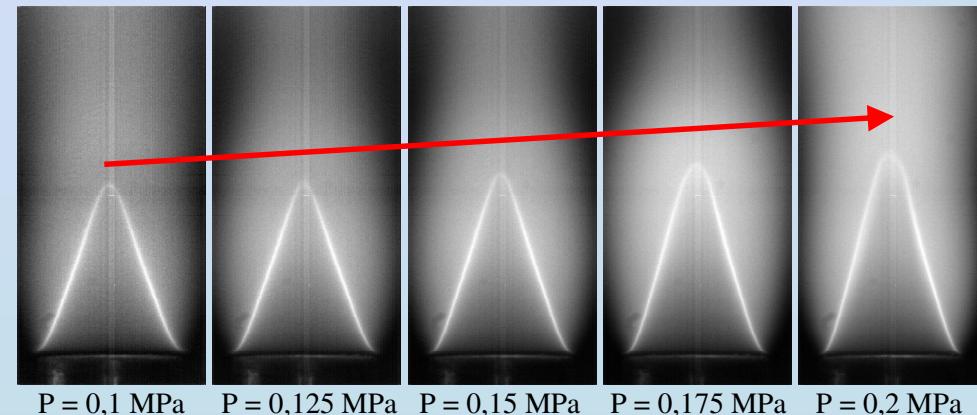
Methodology



- ➡ Camera CCD : 40 Hz – Resolution : 34.8 $\mu\text{m}/\text{pixel}$
- ➡ 500 images for each experimental condition

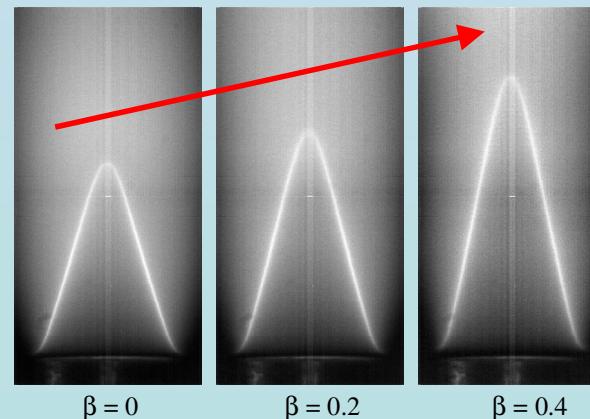
Pressure effect

($U_0=1 \text{ m/s}$ et $\phi = 1$)

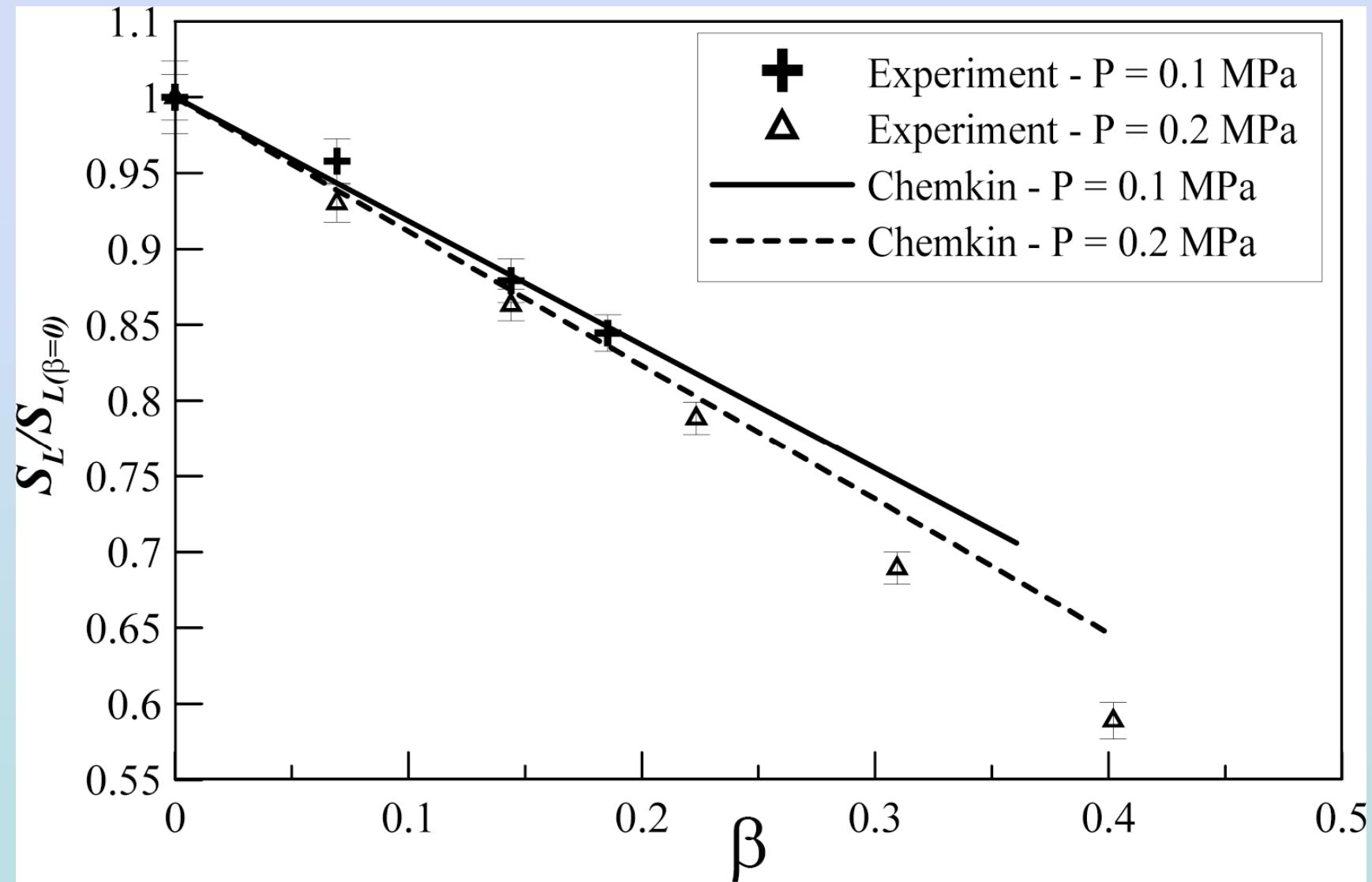


CO₂ addition effect

(P=0.1MPa - $\phi=0.95$ -
 $U_0=1.2\text{m/s}$)



Laminar flame velocities

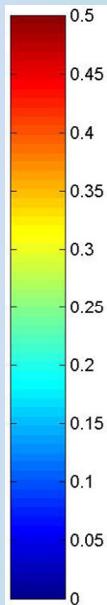
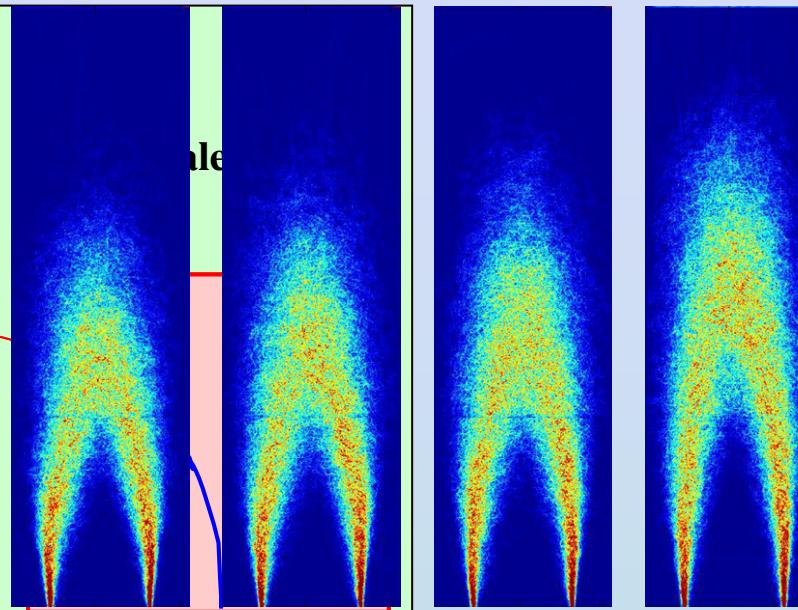
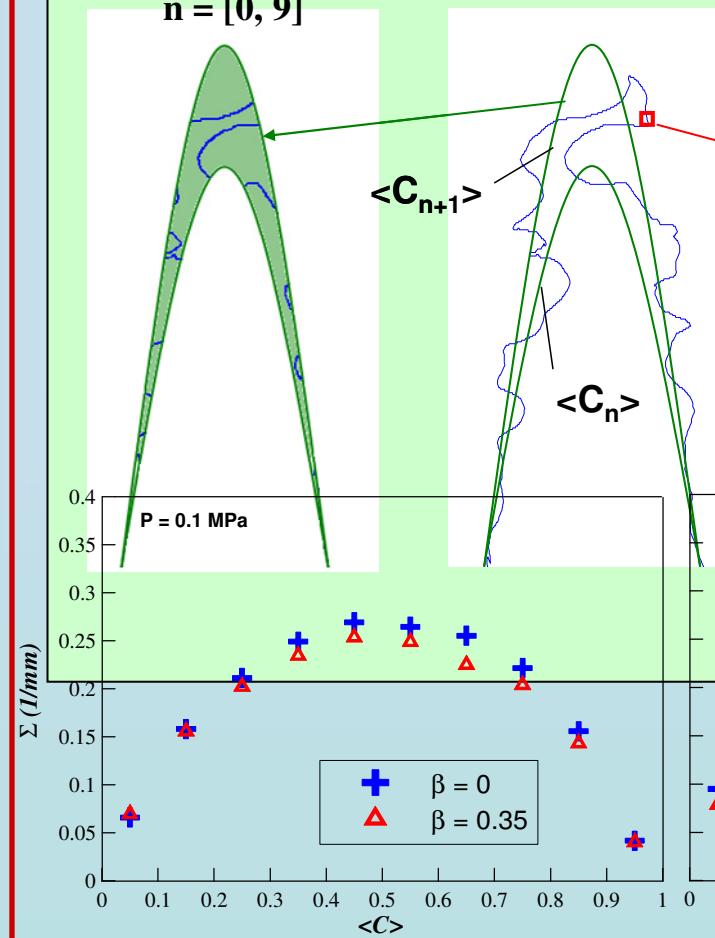


Flame surface density



Determination

Pour $\langle C_{n+1/2} \rangle$
 $n = [0, 9]$



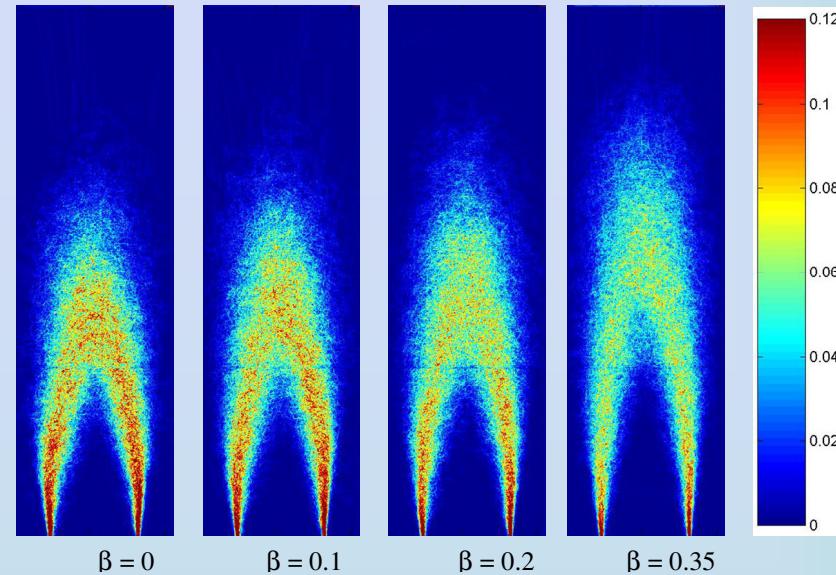
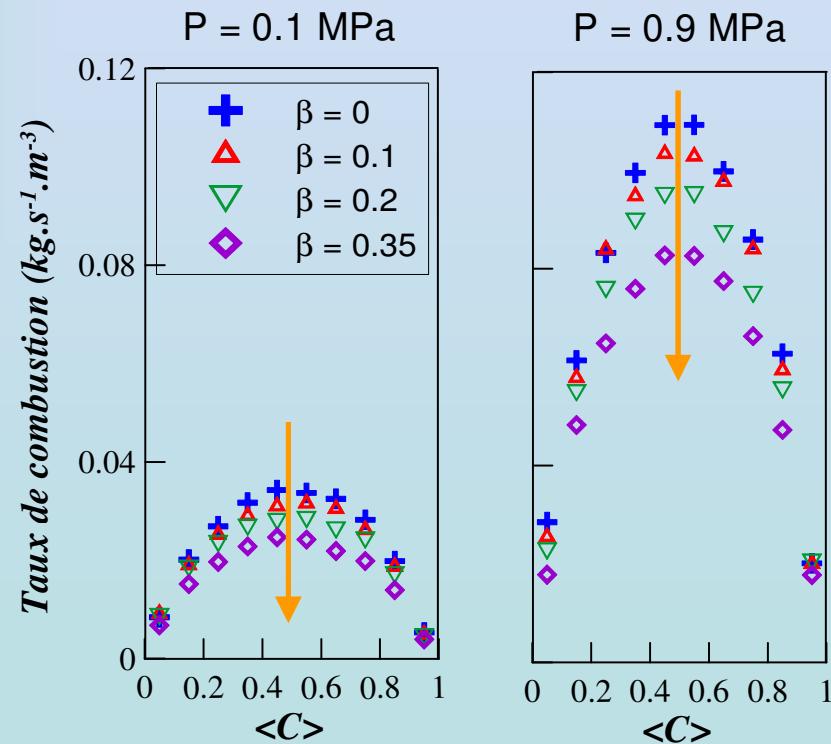
➡ The CO_2 dilution has no effect on the flame surface density.

BML Model



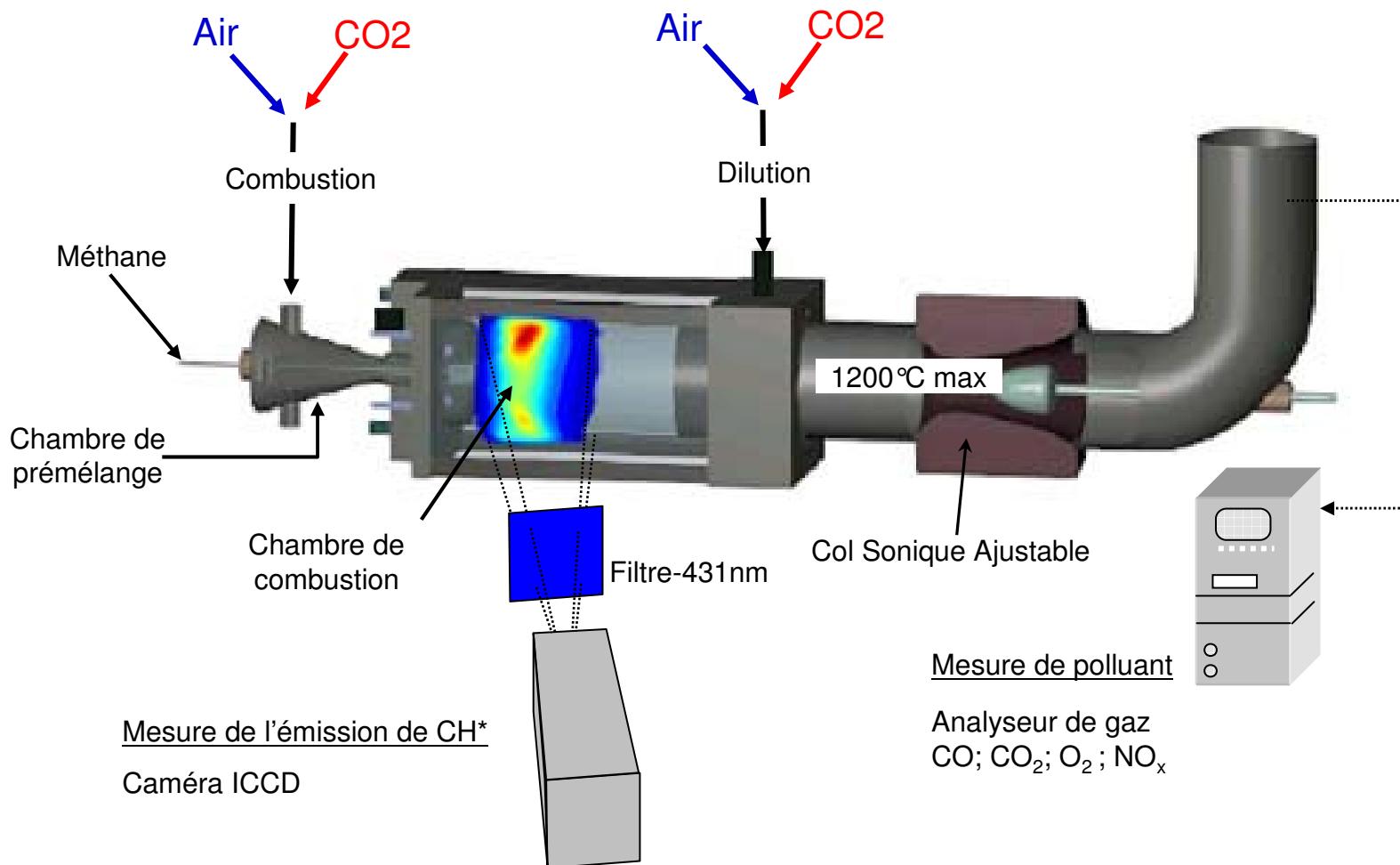
Mean reaction rate

$$\langle w \rangle = \rho_{GF} \cdot S_L^0 \cdot I_0 \cdot \Sigma$$

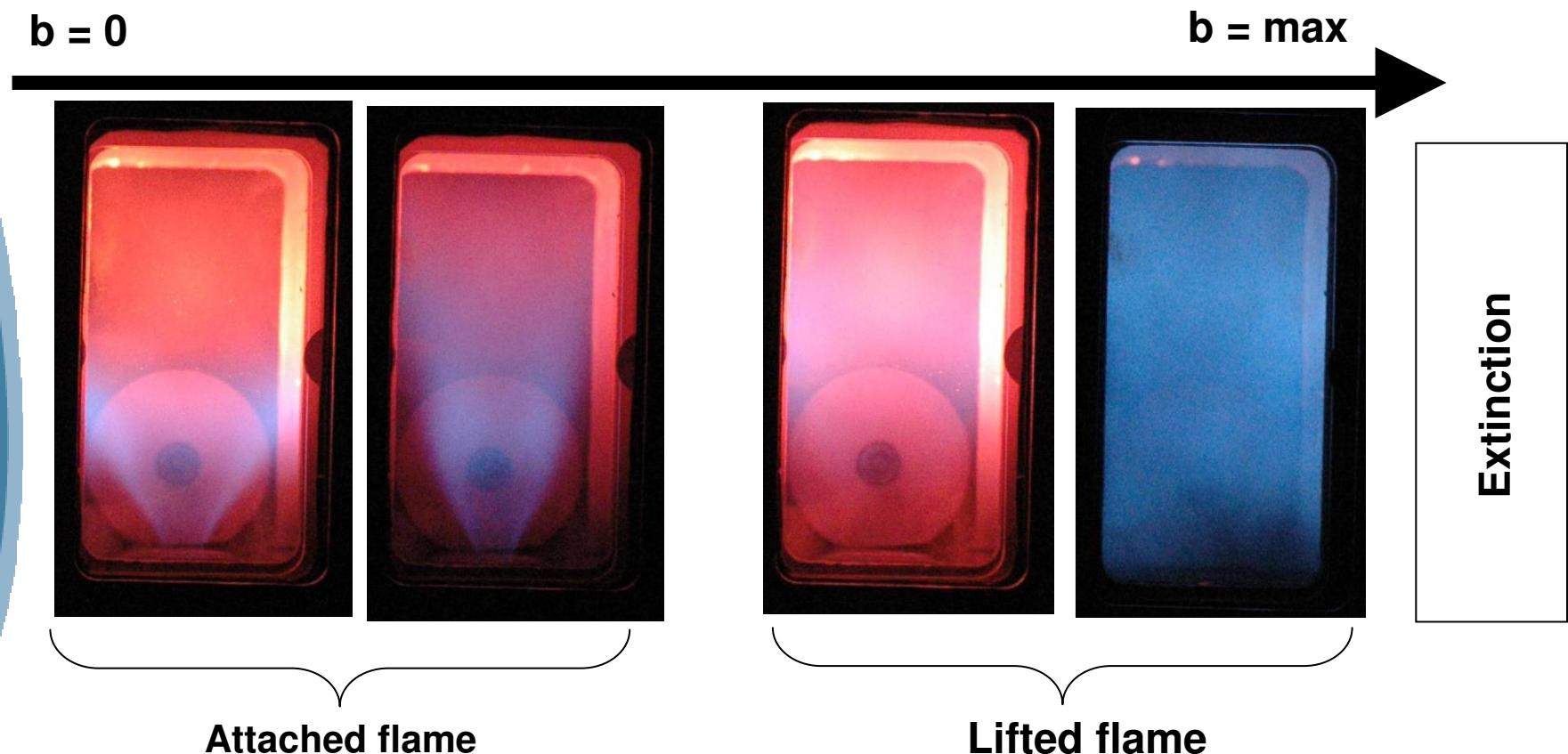


- ▶ Mean fuel consumption rate decrease with the dilution rate
- ▶ Power at $0.1 \text{ MPa} = 2.2 \text{ kW}$
(theoretical = 2 kW)
- ▶ Power at $0.9 \text{ MPa} = 12 \text{ kW}$
(theoretical = 14 kW)

Gas turbine combustion chamber facility of CORIA-CNRS, Rouen



Evolution of turbulent flame structure with CO₂ dilution rate, at constant equivalence ratio



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Topic ENERGY.2008.6.1.3: Efficiency Improvement of Oxygen-based combustion

Content/scope: Further research and demonstration work is needed on oxygen based combustion technologies in respect to the CO₂ capture process to make this technology available for large scale power plants. Work in this area should include – but not be limited to - issues like advanced burner designs as well as slagging, fouling and corrosivity of flue gases, the identification of the optimal CO₂ capture rate, combination of CO₂ capture with other gas cleaning processes and processes for separation, compression and conditioning of CO₂. It is envisaged that a project under this topic will **test, demonstrate and further develop existing technologies in a medium sized test environment**. Scalability of the results to large scale power plants has to be in the focus of the activities.

Funding scheme: Collaborative project with a **dominant demonstration component**.

Expected impact: Oxygen-based combustion technologies can play an important role for CCS. Projects under this topic shall **further develop these technologies and test them in small scale demonstration plants and thereby pave the way for their use in industrial scale power plants**.

Open in call: FP7-ENERGY-2008-2

Why oxy-fuel lignite combustion ?

- To improve the efficiency of lignite combustion; retrofitting possible; rapid benefits for electricity production for countries such as Turkey and Greece
- To ease CO₂ capture
- less NO_x as recycled NO (fuel NO) is burned out and no thermal NO_x (no N₂)
- EOR
- Enhanced CBM

Issues (1)

- Retrofit is possible and demonstrated in pilot scale systems. O₂ is mixed with a fraction (important about 65%) of the flue gases (CO₂ and H₂O mainly or if after condensation mainly only CO₂). This helps to reduce the flame temperature and obtain flame conditions equivalent to air burning. As the CO₂ and H₂O thermal capacities are higher than that of N₂, more O₂ concentration is needed to obtain full conversion. It is possible to adjust the O₂ and flue gas concentration to match the heat transfer parameters to that of air burning

Issues (2)

- As the flow physical parameters are different between air and recycled flue gas and oxygen mixture, if we want to match the heat transfer rate, the flow rates will be different. Therefore a new burner design is necessary
- SO₂ SO₃ emissions may increase, corrosion should be handled
- Heat transfer parameters may also need adjustment; no air in leakage should be allowed, so the boiler should be very well sealed

Issues (3)

- ASU (air separation unit) is the most energy consuming part, 95% O₂ is generally used to reduce the cost penalty
- Also for CO₂ recycling and capture compressors are necessary
- Therefore, oxy-fuel coal burning with CCS gives clearly a lower energy efficiency compared to air burning
- But CCS with air burning and amine based systems is even more costly; then we have to compare comparable issues

Issues (4)

- The efficiency issue should be considered globally. With oxy-fuel combustion we shall burn much more efficiently the lignite. Combustion studies should be done
- Captured CO₂ should be used intelligently: for EOR, for ECBM, for inclusion into cement and concrete production, for ex-situ carbonation etc. We have to increase the value of the whole chain by using CO₂ as a commodity

Issues (5)

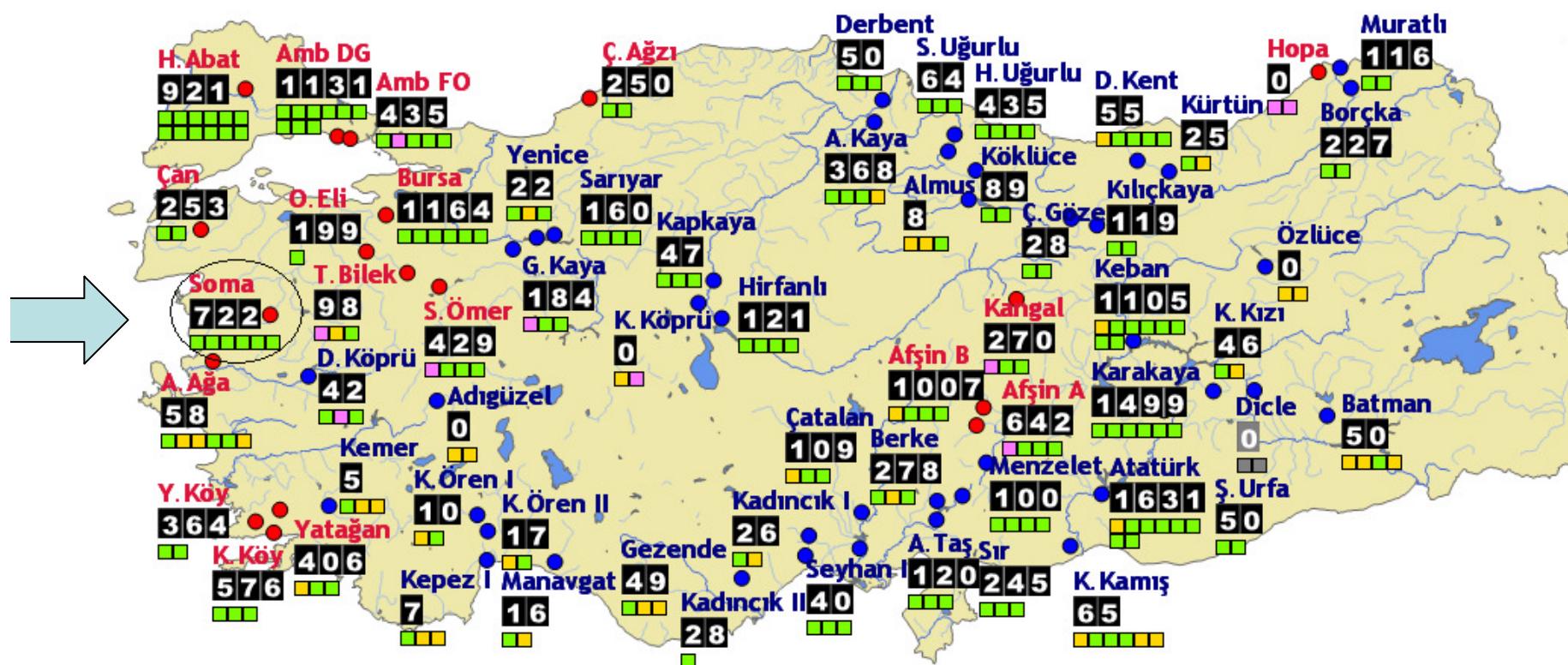
- We need to chose a demonstration site for oxy-fuel lignite combustion: SOMA A: EUAS, TKI
- Compatible power level with the FP7 requirements: 22 MW with several burners of the MW level
- Pulverized lignite with oxy-fuel retrofitting, dissemination and scalability potential
- Enhanced CBM potential in the area...

SOMALOX

- A proposal for FP7 ENERGY TREN 2008 to demonstrate retrofitting the SOMA A pulverized lignite power plant (22 MW) to oxy-fuel combustion
- Partnership: AEE, RWE NPower, CKD Export, ENEA, TKI, EUAS, HABAS, CNRS, NTUA, JRC-IE, Cottbus, Nottingham...

Where is SOMA ?

150 km north-east of Izmir



SOMALOX Work package structure

- WP I: Simulation of the optimisation of the SOMA A power plant for oxy-fuel lignite combustion retrofitting
 - Simulation of the global process
 - Optimisation of the lignite preparation for oxy-fuel combustion
- WP II Optimisation of oxygen production, gas cleaning, CO₂ capture
- WP III Optimisation of the oxy-fuel lignite burner
- WP IV Retrofitting and Demonstration at the plant level
- WP V Economic, Environmental, Dissemination, Scalability analysis

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**THE NINTH ASIA-PACIFIC
INTERNATIONAL SYMPOSIUM
ON COMBUSTION AND
ENERGY UTILIZATION
(9th APISCEU)**

**November 02-06, 2008
Beijing, China**

Organized by
**Beijing Society of Thermophysics and Energy
Engineering, China**
**Institute of Engineering Thermophysics,
Chinese Academy of Sciences**
**Beijing Shenwu Thermal Energy Technology
Co, LTD, China**
**Yanshan Petro-Chemical Industry
Corporation, China**
The Combustion Institute, USA
Sponsored by
**Beijing Association for Science and
Technology, China**

Internet: <http://www.APISCEU9.org.cn>

10th ICCEU

- 10th International Conference on Combustion and Energy Utilisation
- Will be organized at the University of Mugla, Turkey, on 4-8 May 2010
- Main topic: Clean fossil fuel technologies : (technical and socio-economic aspects)
- Contact: Iskender Gökalp
gokalp@cnrs-orleans.fr